

Phase relations in the SrO–SiO₂–ZrO₂ system

I. The system SrO–SiO₂

M. E. Huntelaar, E. H. P. Cordfunke and A. Scheele

Netherlands Energy Research Foundation ECN, Petten (Netherlands)

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Abstract

The phase diagrams of the systems Sr₂SiO₄–SrSiO₃ and SrSiO₃–SiO₂ have been determined experimentally using differential thermal analysis. The eutectic compositions and temperatures of the Sr₂SiO₄–SrSiO₃ and SrSiO₃–SiO₂ subsystems are estimated to be 49.3 mol% SiO₂, 1840 K and 65.8 mol% SiO₂, 1615 K respectively. The enthalpy of fusion of SrSiO₃ has been measured to be 56 ± 6 kJ mol⁻¹.

1. Introduction

When during a severe nuclear reactor accident the core of the reactor melts, interactions of the fission products with the underlying concrete basemat are likely to occur. The formation of new compounds on reaction with the concrete will influence the release of less volatile, radiologically hazardous fission products such as barium or strontium. For this reason and because silica (SiO₂) is one of the main constituents of concrete, the phase diagram of the system SrO–SiO₂ is of particular interest.

Three compounds have been identified in this system: SrSiO₃, Sr₂SiO₄ and Sr₃SiO₅. The phase diagram of the system (or parts of it) has been determined by Eskola [1], Greig [2], Fields *et al.* [3] and Hageman and Oonk [4]. The investigations of Eskola and of Greig cover only the silica-rich side of the system. In addition, Hageman and Oonk measured the liquid immiscibility at this side of the system. Neither Eskola nor Greig was aware of the existence of Sr₃SiO₅, which was first reported by Nurse [5]. According to Eysel [6], Sr₃SiO₅(s) is not stable at room temperature but decomposes into SrO(s) and Sr₂SiO₄(s), similar to the CaO–SiO₂ system. Thermodynamic properties of this compound which could prove this are completely lacking.

The phase diagram analysis by Fields *et al.* covers only the strontium-oxide-rich side of the system. The liquidus curve of strontium oxide as proposed by these authors is not compatible with the melting point of strontium oxide reported by Noguchi [7] and Traverse and Foex [8]. Fields *et al.* adopted the measurements made by Eskola and by Greig for the silica-rich side to construct a phase diagram of the SrO–SiO₂ system.

Since the amount of strontium in irradiated nuclear fuel is small compared with the amount of silica present in the concrete, phase relations in the SrSiO₃–SiO₂ subsystem are of particular interest in nuclear technology. This system is insufficiently known and has therefore been (re)investigated in the present study.

2. Experimental details

The samples used in the differential thermal analysis (DTA) study have been prepared by mixing known amounts of Sr₂SiO₄(s) and SrSiO₃(s) or of SrSiO₃(s) and amorphous SiO₂(s) (Aldrich, 99.995% purity). The pure samples of Sr₂SiO₄(s) and SrSiO₃(s) are the same as used in ref. 9. All mixtures prepared for the SrSiO₃–SiO₂ subsystem were first partly melted at ± 1625 K and then recrystallized at 1550 K in a purified argon atmosphere. Before and after each measurement the samples were analyzed by X-ray diffraction. In all mixtures containing SiO₂, cristobalite was found to be the crystalline phase at room temperature. In some of the mixtures with a high SiO₂ content, small traces of tridymite were found as well.

The DTA measurements were carried out in a Mettler TA 13-2000 apparatus using platinum crucibles. All measurements were made in a purified argon atmosphere to prevent the formation of volatile platinum oxides. The maximum temperature which can be obtained with the DTA furnace is 1873 K. The temperatures were corrected using the melting point of high purity palladium (1825 K) as a reference. Almost all measurements were reproducible within 3 K. The sensitivity of the DTA apparatus was calibrated against

the enthalpies of fusion of silver, gold and palladium. The measurements were performed with ramp speeds between 1 and 25 K min⁻¹.

Quenching experiments were performed using a high temperature furnace. For each quenching experiment a platinum crucible was sealed in a partly evacuated (Ar pressure $\pm 10^4$ Pa), Al₂O₃-stabilized quartz capsule. Before quenching in ice water, the capsule was equilibrated for at least 45 min at the temperature of interest. The temperature was measured using a Pt/Pt–10%Rh thermocouple directly adjacent to the capsule.

Most handlings, such as weighing, were done in an argon-filled glove-box. All masses were corrected for buoyancy in argon.

3. Results

3.1. DTA measurements

The measured solidus and liquidus temperatures of the Sr₂SiO₄–SrSiO₃ and SrSiO₃–SiO₂ subsystems are listed in Table 1. Only a few points in the Sr₂SiO₄–SrSiO₃ subsystem could be measured because of the very high temperatures and the steep liquidus curve of Sr₂SiO₄.

TABLE 1. Solidus and liquidus temperatures in the system SrO–SiO₂

| Sample | SiO ₂ (mol%) | T_{sol} (K) | T_{liq}^a (K) |
|--|----------------------------|-------------------------|---------------------------|
| <i>Sr₂SiO₄–SrSiO₃</i> | | | |
| Sr/Si-53 | 47.50 | 1841 | – |
| Sr/Si-52 | 48.07 | 1840 | – |
| Sr/Si-86 | 49.00 | 1839 | 1861 |
| Sr/Si-87 | 49.12 | 1839 | 1863 |
| <i>SrSiO₃–SiO₂</i> | | | |
| Sr/Si-62 | 50.00 | – | 1853 |
| Sr/Si-77 | 52.00 | 1619 | 1855 |
| Sr/Si-72 | 54.06 | 1609 | 1833 |
| Sr/Si-75 | 56.00 | 1614 | 1805 |
| Sr/Si-70 | 58.28 | 1616 | 1767 |
| Sr/Si-64 | 58.41 | 1614 | 1758 |
| Sr/Si-65 | 58.96 | 1616 | 1751 |
| Sr/Si-66 | 59.49 | 1610 | 1747 |
| Sr/Si-71 | 60.61 | 1616 | 1722 |
| Sr/Si-76 | 62.00 | 1619 | 1695 |
| Sr/Si-67 | 64.39 | 1617 | 1654 |
| Sr/Si-73 | 65.20 | – | 1632 |
| Sr/Si-74 | 65.99 | 1617 | – |
| Sr/Si-79 | 67.01 | 1618 | – |
| Sr/Si-84 | 67.96 | 1614 | – |
| Sr/Si-83 | 69.00 | 1616 | 1708 |
| Sr/Si-85 | 69.50 | 1614 | 1739 |
| Sr/Si-80 | 69.98 | 1615 | 1749 |
| Sr/Si-81 | 71.01 | 1615 | 1760 |
| Sr/Si-82 | 72.01 | 1621 | 1787 |

^aAll errors are within 1–3 K, except for the sample Sr/Si-85 where the liquidus temperature has an error of 18 K.

Temperatures on the SiO₂ branch of the SrSiO₃–SiO₂ system were difficult to measure owing to the relatively small enthalpy of fusion of SiO₂.

The melting temperature of pure SrSiO₃ was found to be 1853 ± 5 K, which is in excellent agreement with previous measurements by Jaeger and Van Klooster [10] (1851 ± 1 K), Eskola [1] (1853 ± 4 K) and Fields *et al.* [3] (1853 ± 15 K). For the melting temperature of SrSiO₃ the value 1853 ± 4 K is suggested.

3.2. Enthalpy of fusion

The enthalpy of fusion of SrSiO₃ was very difficult to obtain because the melting temperature lies only 20 K below the maximum obtainable temperature of our DTA apparatus. Another problem was the determination of the area under the melting peak. Owing to $\Delta_{\text{fus}}C_p$, the baseline leaps and therefore the peak area could not be determined unequivocally. Values between 50 and 62 kJ mol⁻¹ were calculated depending on the calculational method applied. For the enthalpy of fusion of SrSiO₃ the value 56 ± 6 kJ mol⁻¹ is therefore suggested.

3.3. Phase relations

The crystal structure of SrSiO₃ is monoclinic as reported by Machida *et al.* [11] and Marsh and Herbststein [12]. We found that on addition of even small amounts of SiO₂ the crystal structures became a little distorted, indicating that a small solubility area for SiO₂ may exist. The size of this solubility region has not been established in this study and so will be disregarded here.

In all our attempts to obtain tridymite as a stable phase, cristobalite was found as the major SiO₂ phase. Experiments were performed in which several mixtures of SrO(s) and SiO₂ were heated to 1573 K for a 240 h period. In these experiments tridymite was not found after slow cooling to room temperature. A similar experiment with CaO(s) and SiO₂ also yielded cristobalite only. This is in contrast to our experiments with SiO₂ and Na₂O, in which tridymite was readily obtained.

Quenching experiments at higher temperatures were performed with the sample Sr/Si-80 (molar ratio SrO:SiO₂=0.4290) to establish the phase relations at higher temperatures. A quenching experiment at 1600 K yielded tridymite, cristobalite and SrSiO₃ as the crystalline phases, whereas at 1640 K only tridymite could be found in the partially molten sample. Equilibria at still higher temperatures could not be measured because the capsules started to deform at 1640 K. The presence of tridymite in the quenched samples indicates that at higher temperatures the tridymite phase does exist. However, if mixtures are cooled down slowly from the same temperatures (1625–1640 K), only SrSiO₃,

cristobalite and sometimes a small amount of tridymite are obtained.

It can be concluded from these experiments that although tridymite is formed in the liquid, the formation of cristobalite is kinetically more favourable. The presence of tridymite or cristobalite will, however, hardly effect the activities in the system, because the energy differences between the two phases are extremely small [13]. For this reason and because of the fact that tridymite is not a stable phase of pure (unstabilized) SiO₂ [14], the tridymite ↔ cristobalite transition (± 1743 K) will be disregarded here.

4. Discussion

Our DTA measurements show that previous measurements in the SrSiO₃–SiO₂ system by Eskola and by Greig, who determined only a few points using a quenching method, are in fair agreement with the present results. According to our findings, the eutectic point in the SrSiO₃–SiO₂ system is situated at 1615 ± 3 K and 65.8 mol% SiO₂, which is only slightly different from the 1631 K and 66.49 mol% SiO₂ obtained by Eskola. In Fig. 1 a new phase diagram of the SrSiO₃–SiO₂ system is presented; the Sr₂SiO₄–SrSiO₃ system is given in the inset. The tridymite ↔ cristobalite transition temperature (1743 K) has been taken from the assessment of Wriedt [14].

In the Sr₂SiO₄–SrSiO₃ subsystem the eutectic point is found to be situated at approximately 1840 ± 3 K and 49.3 mol% SiO₂. These results are different from the results obtained by Eskola and by Fields *et al.*, who found 1818 K, 46.4 mol% SiO₂ and 1818 K, ± 47 mol% SiO₂ respectively. The lower temperature found by

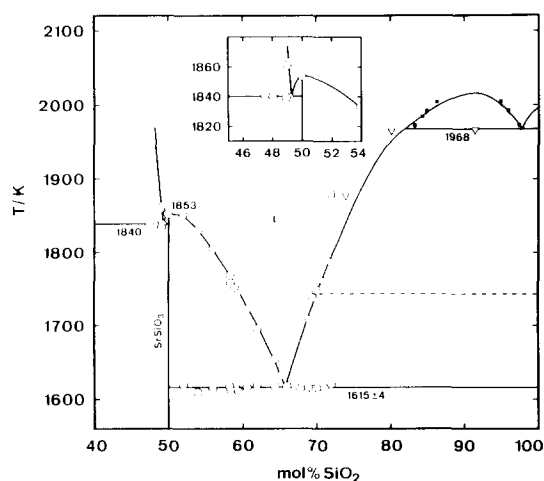


Fig. 1. The experimental phase diagram of the SrSiO₃–SiO₂ system. Inset: the eutectic region of the Sr₂SiO₄–SrSiO₃ phase diagram. Symbols: □, Eskola [1]; ▽, Greig [2]; ■, Hageman and Oonk [4]; ○, present study.

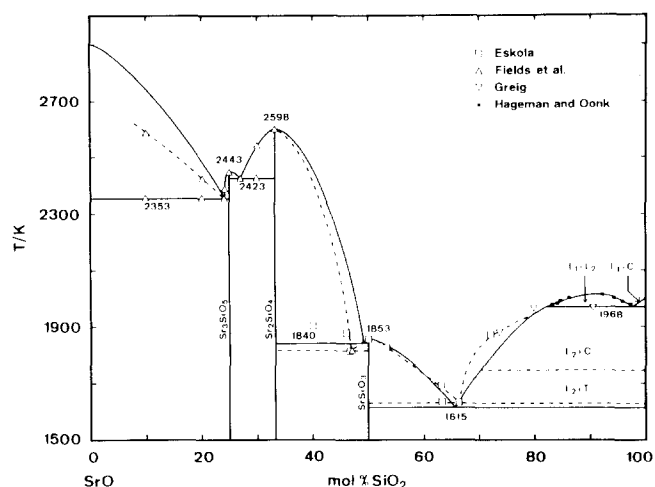


Fig. 2. The assessed phase diagram of the SrO–SiO₂ system: C, cristobalite; T, tridymite. The dashed lines indicate the previous phase equilibria.

TABLE 2. Melting points, eutectic temperatures and eutectic compositions in the system SrO–SiO₂

| Compound | T_{melt} (K) | T_{eut} (K) | X_{eut} (mol% SiO ₂) |
|----------------------------------|--------------------------|-------------------------|--|
| SrO | 2900 | | |
| Sr ₃ SiO ₅ | 2443 | 2353 | ~ 23 |
| Sr ₂ SiO ₄ | 2598 | 2423 | ~ 27 |
| SrSiO ₃ | 1853 | 1840 | 49.3 |
| SiO ₂ | 1996 | 1615 | 65.8 |

Fields *et al.* can probably be explained by the use of the oxygen–acetylene torch, which might have resulted in the formation of hydroxides.

An assessed phase diagram of the whole SrO–SiO₂ system is given in Fig. 2. The liquidus measurements by Fields *et al.* on the SrO-rich side are possibly subject to errors, since they are in serious disagreement with the determinations of the melting point of SrO by Noguchi [7] (2872 ± 20 K) and Traverse and Foex [8] (2938 ± 20 K). We here select the value 2900 ± 40 K for the melting point of strontium oxide, *i.e.* the mean of the values of the latter two authors. A list of melting points, eutectic temperatures and eutectic compositions is given in Table 2.

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